

Inversion of two-flux and four-flux radiative transfer models in WO₃-NiO electrochromic devices

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Inversión de los modelos de transferencia radiativa de dos flujos y de cuatro flujos en dispositivos electrocrómicos de WO₃-NiO

Abstract

Intrinsic and extrinsic scattering and absorption coefficients (S&A-C) of four inorganic electrochromic device (ECD) samples were determined at their bleached-off optical state (BOOS, 0 V) and at their colored-on optical state (COOS, +3 V DC). The same inversion procedure previously applied to suspended particle device (SPD) and polymer-dispersed liquid crystal (PDLC) samples, approximated for a single layer sandwich structure, was used here for a third smart window technology, based on redox reactions. The four studied ECDs incorporated cathodic WO₃ and anodic NiO layers corresponding to the four possible combinations of two thicknesses for each material—single (120 nm) and double (240 nm)—within their sandwich structures. The analysis of their S&A-C was performed in three stages. First, determination of optical constants using the collimated solutions of the four-flux model (4FM) from collimated transmittance and reflectance (T&R) measurements. Second, estimation of extrinsic S&A-C from the two-flux model (2FM) using total (collimated + diffuse) T&R data. Third, extraction of intrinsic S&A-C from the diffuse 4FM solutions by means of diffuse T&R data, employing the diffuse interface reflectance, an approximate average crossing parameter, and the forward scattering ratio. Although light scattering was found to be weak, absorption for the COOS showed a clear dependence on the WO₃-NiO active layers thicknesses: neutral gray ECD11 (single WO₃-single NiO), brownish gray ECD12 (single WO₃-double NiO), bluish gray ECD21 (double WO₃-single NiO), and dark gray ECD22 (double WO₃-double NiO). As expected, similar optical appearances were observed in the BOOS for the four ECDs. The values weighted by the CIE 1931 standard observer color matching function (\bar{y}) indicate that increasing the WO₃ thickness twofold leads to a larger absorption coefficient increment than a twofold increase in the NiO thickness. The single-layer 4FM implementation adopted in this study provides reliable agreement in the 250–1500 nm wavelength range, while fitting inaccuracies appear beyond 1500 nm (i.e., in the 1500–2500 nm region) between the calculated and the measured diffuse transmittance at BOOS, for ECD11 and ECD22, and at COOS, for ECD11. No fitting inaccuracies were observed between the calculated and the measured diffuse reflectance. Concerning the 2FM study, an excellent agreement in fitting was observed between the calculated and the measured total T&R for the four ECD samples.

Keywords: optical constants, average crossing parameter, forward scattering ratio, diffuse fractions of light, extinction, intrinsic and extrinsic coefficients, smart windows.



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Resumen

Los coeficientes de dispersión y absorción (S&A-C) intrínsecos y extrínsecos de cuatro muestras de dispositivo electrocrómico (ECD) inorgánico fueron determinados en su estado óptico aclarado-apagado (BOOS, 0 V) y en su estado óptico coloreado-encendido (COOS, +3 V CC). El mismo procedimiento de inversión previamente aplicado con muestras de un dispositivo de partículas suspendidas (SPD) y de cristales líquidos dispersos en polímero, aproximado para una estructura sándwich de una única capa substrato, fue aquí utilizado para una tercera tecnología de ventanas inteligentes, basada en reacciones redox. Los cuatro ECD estudiados incorporaron capas catódicas de WO_3 y capas anódicas de NiO correspondientes a las cuatro combinaciones posibles de dos espesores para cada material —simple (120 nm) y doble (240 nm)— dentro de sus estructuras tipo sándwich. El análisis de sus S&A-C se realizó en tres etapas. Primero, determinación de las constantes ópticas usando las soluciones colimadas del modelo de cuatro flujos (4FM) y considerando las medidas de transmitancia y reflectancia (T&R) colimadas. Segundo, estimación de los S&A-C extrínsecos a partir del modelo de dos flujos (2FM) usando los datos de T&R totales (colimados + difusos). Tercero, extracción de los S&A-C intrínsecos a partir de las soluciones difusas del 4FM mediante los datos de T&R difusos, empleando la reflectancia difusa de interface, un parámetro de camino promedio aproximado, y el porcentaje de dispersión hacia adelante. Aunque la dispersión de luz resultó ser débil, la absorción para los COOS mostró una dependencia clara con el espesor de las capas activas $\text{WO}_3\text{-NiO}$: ECD11 gris neutro (simple $\text{WO}_3\text{-simple NiO}$), ECD12 gris con un tinte marrón (simple $\text{WO}_3\text{-doble NiO}$), ECD21 gris con un tinte azul (doble $\text{WO}_3\text{-simple NiO}$) y ECD22 gris oscuro (doble $\text{WO}_3\text{-doble NiO}$). Como se esperaba, se observaron apariencias ópticas similares para los BOOS de los cuatro ECDs. Los valores ponderados por la función de correspondencia de color del observador estándar CIE 1931 (\bar{y}) indican que aumentar el espesor de WO_3 al doble conduce a un incremento del coeficiente de absorción mayor que un aumento del doble del espesor de NiO. La implementación de 4FM de una sola capa adoptada en este estudio proporciona un acuerdo confiable en el rango de longitud de onda de 250 a 1500 nm, mientras que aparecen imprecisiones de ajuste más allá de los 1500 nm (es decir, en la región de 1500 a 2500 nm) entre la transmitancia difusa calculada y medida en el BOOS, para los ECD11 y ECD22, y en el COOS, para el ECD11. No se observaron imprecisiones de ajuste entre la reflectancia difusa calculada y medida. Respecto al estudio del 2FM, se observó un acuerdo excelente en el ajuste entre la T&R totales calculadas y medidas para las cuatro muestras de ECD

Palabras clave: constantes ópticas, parámetro de camino promedio, porcentaje de dispersión hacia adelante, fracciones difusas de la luz, extinción de la luz, coeficientes intrínsecos y extrínsecos, ventanas inteligentes.

INTRODUCTION

Chromogenic electrochromic devices (ECDs) regulate the amount of transmitted light by applying an external electric potential, making them key components of smart window technologies. The energy consumption for heating, cooling and lighting of buildings (which is around 30-40% of the primary energy used in the world) can be reduced by using smart windows technologies [1]. These devices exhibit two optical

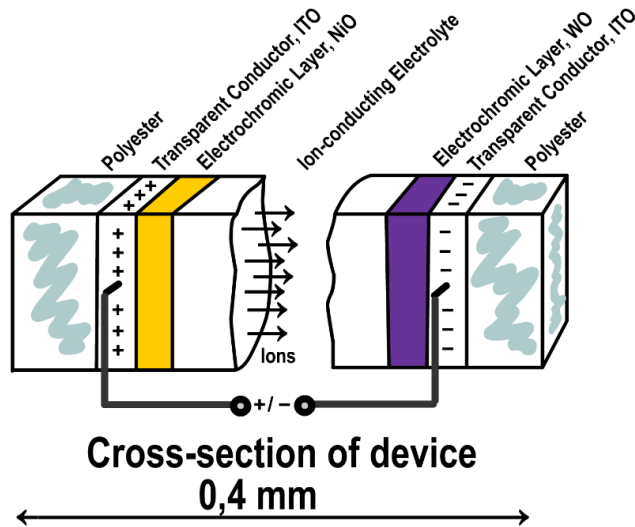


FIGURE 2. Sandwich structure of inorganic EC smart windows based on tungsten oxide, nickel oxide, and indium tin oxide (ITO) transparent conductors [2].

However, thin films are not considered in this study, which focuses on a single-layer (substrate) approximated analysis of four $\text{WO}_3\text{-NiO}$ ECDs using the procedure established in previous works [13, 14, 15]. The same methodology was previously applied to the SPD sample [13]—analyzed at dark-off and clear-on states—and to polymer-dispersed liquid crystal (PDLC) samples [14, 15]—analyzed at translucent-off and transparent-on states. Each sample contains WO_3 and NiO active layers deposited on FTO-coated glass, separated by an electrolyte substrate layer (Fig. 2). The four ECD were characterized for both BOOS and COOS. Collimated, diffuse, and total transmittance (T) and reflectance (R) measurements (T&R-M) were used to determine the OC and the intrinsic and extrinsic S&A-C through the single-layer approach described in [13, 14, 15].

The main contribution of this work, compared with previous studies, lies in evaluating the applicability of the single-layer procedure previously employed for SPD and PDLC samples [13, 14, 15]—where both scattering and absorption occur (with absorption dominating in SPD and scattering in PDLC)—to samples in which scattering is nearly negligible and absorption clearly predominates, such as ECDs. The optical characterization process carried out involves three main stages:

A. First stage: Determination of OC from collimated T&R components

Real (n) and imaginary (k) parts of the complex refractive index ($\tilde{n} = n - i\kappa$) or OC are obtained from the collimated T&R-M, i.e., the regular T (T_{reg}) and specular R (R_{spe}). From the OC, the complex Fresnel reflection coefficient is calculated, and its squared modulus yields the collimated interface reflectance (r_c), obtaining the same values for external (r_c^e) and internal (r_c^i) components, i.e., a single r_c value for both propagation directions ($r_c^e = r_c^i$). Since all measurements were taken at normal incidence, polarization averaging



is unnecessary. The extinction coefficient (ϵ), related to both scattering and absorption, depends on κ and the wavelength (λ) as $\epsilon = 4\pi\kappa/\lambda$, resulting in the collimated substrate layer attenuation $\tau_c = \exp(-\epsilon \cdot dz)$.

B. Second stage: Estimation of extrinsic S&A-C (S & K) from total T&R components

The Kubelka–Munk two-flux model (KM-2FM) [16] with Saunderson correction [17] is applied to account for interface effects. Analytical hyperbolic solutions for R [16] and for T [18] were used with total T&R-M. Although the KM-2FM was initially formulated for diffuse T (T_{dif}) and R (R_{dif}), samples exhibiting both collimated and diffuse components are analyzed using total values ($T_{tot} = T_{reg} + T_{dif}$, $R_{tot} = R_{spe} + R_{dif}$) [19]. Diffuse light fractions (q) are employed to compute the total interface reflectance $\omega = r_c(1-q) + r_d q$, where r_d is the diffuse interface reflectance. Two distinct ω values (ω^i and ω^j) appear at the front ($z = \delta$) and back ($z = 0$) interfaces, corresponding to forward (i) and backward (j) propagation, respectively (using q^i and q^j). For external illumination only from the front interface ($i^\delta = i_c^\delta = 1$), $q^j = 0$, and therefore q^i and ω^i are not required. The expressions for q^i and q^j were originally derived from SPD data [20, 21]. In [13], a fitting discrepancy observed in the visible range for R_{tot} [20, 21] was corrected following a suggestion by David MacAdam (Kodak) to Kottler [22], introducing the critical internal reflection angle (θ_c) as the upper integration limit for computing r_d [23]. Earlier works had integrated up to 90° [19, 24, 25], obtaining different values for external (r_d^e) and internal (r_d^i) components. However, using θ_c instead of 90° yielded a single r_d value for both propagation directions ($r_d^e = r_d^i$), analogous to r_c ($r_c^e = r_c^i$), which resolved the 2FM inconsistencies and enabled the accurate determination of the intrinsic coefficients.

C. Third stage: Extraction of intrinsic S&A-C (α and β) from diffuse T&R components

The Maheu–Letoulozan–Gouesbet four-flux model (MLG-4FM) [26] is applied using the diffuse T&R-M (T_{dif} and R_{dif}). The average crossing parameter (ACP) was approximated in [27, 28, 29] using collimated and diffuse intensities at the interfaces: $ACP = 1 + (i_d^0 + j_d^\delta) / (i_c^0 + i_d^0 + j_c^\delta + j_d^\delta) = 1 + (i_d^0 + j_d^\delta) / (i^0 + j^\delta)$, with $i^0 = i_c^0 + i_d^0$ and $j^\delta = j_c^\delta + j_d^\delta$ representing total intensities. The absorption coefficient (α) and forward scattering ratio (FSR) are determined in a fitting process, and β follows from $\epsilon = \alpha + \beta$. The consistency between 2FM and 4FM solutions is verified through feedback relations between ACP and FSR (ACP_{fb} and FSR_{fb}) according to Vargas's expressions [30]. The same four WO₃-NiO ECDs analyzed here were also studied in [31] using a simplified estimation of ACP and FSR: $ACP = 1 + (T_{dif} + R_{dif}) / (T_{tot} + R_{tot})$, $FSR = T_{dif} / (T_{dif} + R_{dif})$, later referred to as the RT-method in [32].

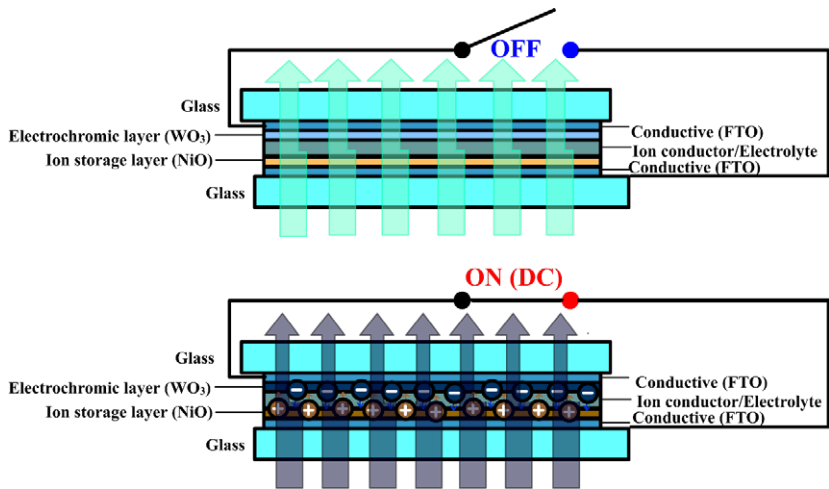


FIGURE 3. Sandwich structure and principle of operation of an inorganic $\text{WO}_3\text{-NiO}$ based ECD smart window at BOOS (above) and COOS (below) [33].

MATERIALS AND METHODS

The optical T&R-M of four $\text{WO}_3\text{-NiO}$ -based ECD samples—designated as ECD11 (single WO_3 -single NiO), ECD12 (single WO_3 -double NiO), ECD21 (double WO_3 -single NiO), and ECD22 (double WO_3 -double NiO)—were performed in [31, 33] and are reused in this study following the same analytical procedure described in [13, 14, 15]. The novelties obtained for the $\text{WO}_3\text{-NiO}$ -based ECD samples are related to the second and third stages, i.e., for determining the intrinsic and extrinsic S&A-C, due to the θ_c limit of the integration used to determine r_d (not used in previous procedure [21, 22]). These samples and their measurements were conducted at the Laboratory for Spectroscopy of Materials at the National Institute of Chemistry, Ljubljana, Slovenia. The ECDs share the same sandwich-type configuration as shown in Fig. 3 [33], consisting of TC electrodes, two EC films (WO_3 and NiO), and an electrolyte substrate layer. The COOS was achieved by applying a +3 V DC bias, while the BOOS was obtained either at 0 V (open circuit, high impedance) or by applying -3 V DC. Optical characterization was performed using a Perkin Elmer Lambda 950 spectrophotometer equipped with an integrating sphere, which allowed the collection of the diffuse components of both T&R. Total and diffuse T&R-M were recorded across the SWR, from 250 to 2500 nm, with a spectral step of 5 nm. The collimated T&R components were then obtained by subtracting the diffuse T&R-M from the total T&R-M.

In addition to these measurements—used later in the Results section—an extra set of measurements was taken with another spectrometer without an integrating sphere, to acquire the collimated transmitted light intensity through the samples. These data were used to compute the direct T ($T_{\text{dir}}=T_{\text{reg}}$) for the separated WO_3 and NiO active layers [31, 33]. These additional measurements were performed on glass-FTO- WO_3 and glass-FTO-NiO samples, which were not assembled into complete devices. Instead, they were placed in a cell containing a liquid electrolyte to independently achieve optical switching between BOOS and COOS. Fig. 4 presents the T_{dir} spectra for WO_3 (a), NiO (b), and the calculated



WO₃-NiO combination (c) at both optical states. Since for two interfaces “A” and “B” and light propagating in forward (i) and backward (j) directions, $T_{AB}^i = T_A^i \cdot T_B^i / (1 - R_A^i \cdot R_B^i)$, this expression can be approximated as $T_{AB}^i = T_A^i \cdot T_B^i$ if $R_A^i = R_B^i = 0$. This approximation was applied because R_{spe} for the separated WO₃ and NiO active layers could not be measured with the experimental setup used for T_{dir} . Fig. 4(d) shows the colorimetric results for the spectra in panels (a)–(c). ECD11 and ECD12 contain single WO₃, while ECD11 and ECD21 include single NiO. ECD21 and ECD22 use double WO₃, and ECD12 and ECD22 use double NiO. Consequently, the approximate colors of ECD11 and ECD22 correspond to neutral grey and dark neutral grey, respectively (due to the doubled active-layer thickness), whereas ECD21 appears bluish neutral grey and ECD12 shows a brownish neutral grey tone.

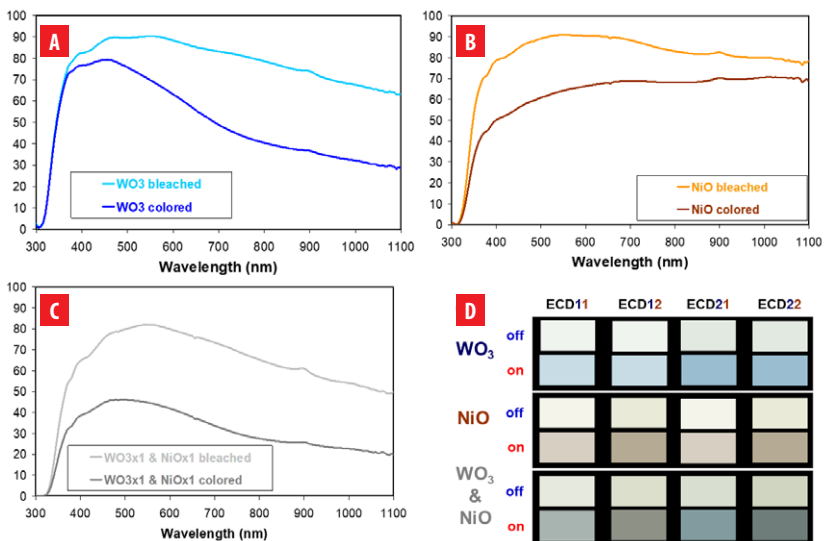


FIGURE 4: Direct transmittance of separated active layers used in the ECD smart window samples: **A** WO₃, **B** NiO, **C** approximated WO₃-NiO and **D** sRGB coloration appearances determined from CIE Yxy 1931 chromaticity coordinates. In the four subfigures, at BOOS and COOS [31, 33].

RESULTS

As outlined in the Introduction, the same methodology previously applied to SPD and PDLC samples [13, 14, 15] was used here to characterize four WO₃-NiO ECDs with two different active-layer thicknesses (120 nm and 240 nm) of their active layers WO₃ and NiO, for both BOOS and COOS. In Figures 5, 6, 7, 8, 9, 10, 11, 12, 13, the four ECD samples—ECD11, ECD12, ECD21, and ECD22—are labeled as samples 1–4, respectively.

A. First stage: Determination of OC from collimated T&R components

The collimated T&R-M and their fittings for the four ECDs in both BOOS and COOS are shown in Fig. 5. The agreement between measured and fitted data is excellent for both optical states. A higher contrast is observed in T_{reg} (Fig. 5a) than in R_{spe} (Fig. 5b). In the COOS, T decreases markedly, while R increases slightly across the visible range. The intermediate



parameters r_c and ε were derived from the MLG-4FM [19] cc equations (Fig. 6). These were obtained by fitting the computed T_{cc} and R_{cc} values to the experimental T_{reg} and R_{spe} data. As expected, r_c (Fig. 6a) correlates more closely with R_{spe} , whereas the attenuation term τ_c (Fig. 6b) is primarily associated with T_{reg} . The ε coefficients are higher in the COOS than in the BOOS, consistent with the EC response.

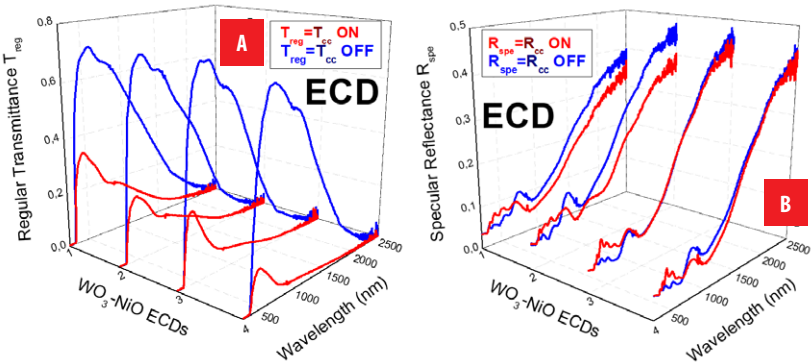


FIGURE 5: Collimated results: T&R-M and fittings. A T_{reg} and T_{cc} . B R_{spe} and R_{cc} .

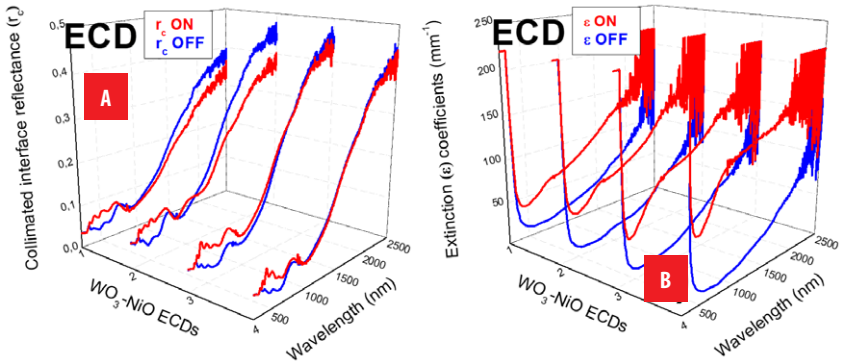


FIGURE 6: Collimated intermediate parameters: A r_c . B ε coefficients (mm^{-1}).

B. Second stage: Estimation of extrinsic S&A-C (S & K) from total T&R components

The fitted total T and R (T_t and R_t) are compared with the measured T_{tot} and R_{tot} in Fig. 7. Note that almost all light transmitted and reflected by the ECDs is collimated, causing the similarities between T_{reg} (Fig. 7a) and T_{tot} (Fig. 5a) and between R_{spe} (Fig. 7b) and R_{tot} (Fig. 5b). The resulting extrinsic coefficients S and K are displayed in Fig. 8. As expected for ECDs with low optical haze, S (Fig. 8a) remains lower than K (Fig. 8b). Fig. 9a shows q_0^i and q_0^j , while Figure 9b presents ω_0^i and ω_0^j . The strong inequality $q_0^j \gg q_0^i$ reflects the fact that, in the backward direction (j) at the front interface (δ), light crosses the internal turbid layer twice, whereas in the forward direction (i) at the rear interface (O), it traverses it only once. Fig. 10a displays the refractive index n , and Fig. 10b the corresponding r_d , which describes the diffuse reflection behavior at the interfaces.

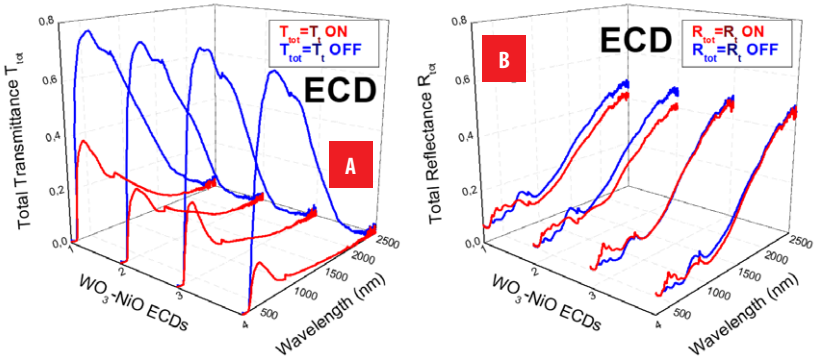


FIGURE 7: Total results: T&R-M and fittings. **A** T_{tot} and T_t ; **B** R_{tot} and R_t .

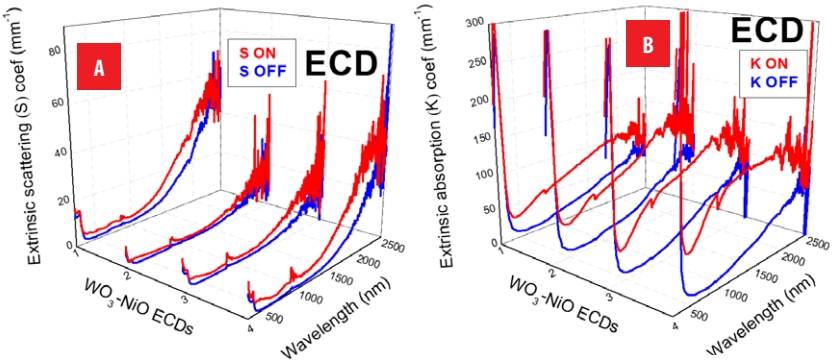


FIGURE 8: Extrinsic S&A-C (mm⁻¹): **A** S and **B** K coefficients.

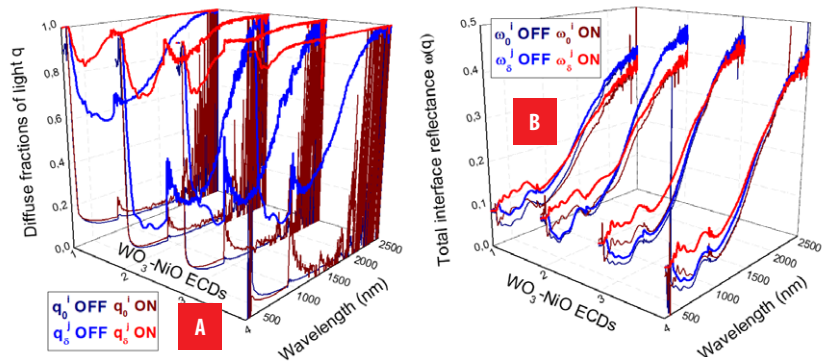


FIGURE 9: **A** Diffuse fractions of light q and **B** total interface reflectance ω .

C. Third stage: Extraction of intrinsic S&A-C (α and β) from diffuse T&R components

The diffuse T&R-M and their fittings to the MLG-4FM [19] cd equations are shown in Fig. 11 for both optical states. The intrinsic coefficients α and β are presented in Fig.



12. As observed for the extrinsic coefficients, α (Fig. 12a) remains lower than β (Fig. 12b), consistent with the low haze of the ECDs. The fittings are excellent over most of the SWR. Deviations are observed exclusively in the T_{dif} of ECD11 and ECD22 at BOOS and of ECD11 at COOS, starting at approximately 1500 nm. Above approximately 2000 nm, an additional increase in fluctuations is observed in T_{dif} , while R_{dif} and all collimated and total components remain unaffected over the entire spectral range. This deviation also appears in Fig. 13, where differences between the fitted and feedback (fb) ACP (Fig. 13a) and FSR (Fig. 13b) values become more pronounced above 1500 nm.

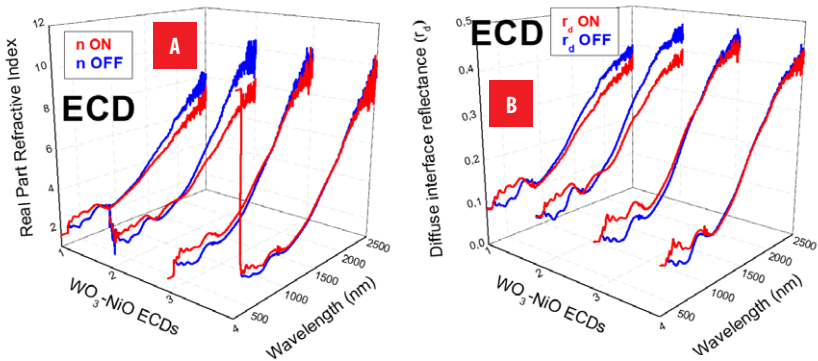


FIGURE 10: A Real part of refractive index n and **B** diffuse interface reflectance r_d .

For improved clarity, the fittings of the collimated, diffuse, and total T&R measurements to the calculated values obtained using the 4FM (collimated T&R in Fig. 5 and diffuse T&R in Fig. 7) and the 2FM (total T&R in Fig. 11), for both BOOS and COOS, are presented in Fig. 17 (transmittance) and Fig. 18 (reflectance). The only discrepancies between calculated and measured data are observed in the diffuse transmittance for ECD11 and ECD22 at BOOS, and for ECD11 at COOS, consistently within the wavelength range of 1500–2500 nm. The fitting error within the 250–1500 nm range is negligible compared to the experimental uncertainty.

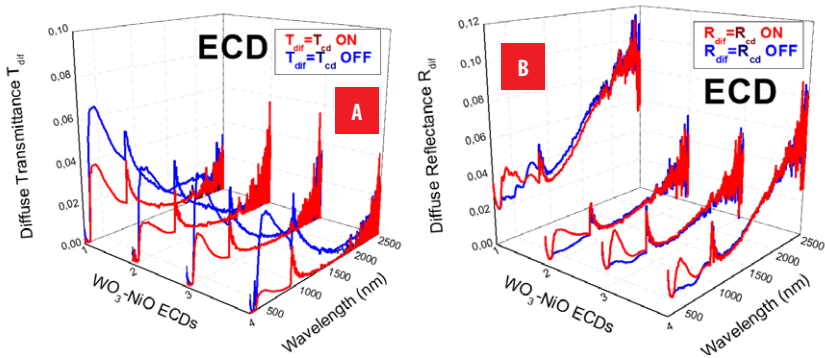


FIGURE 11: Diffuse results: T&R-M and fittings. A T_{dif} and T_{cd} and **B** R_{dif} , and R_{cd} .

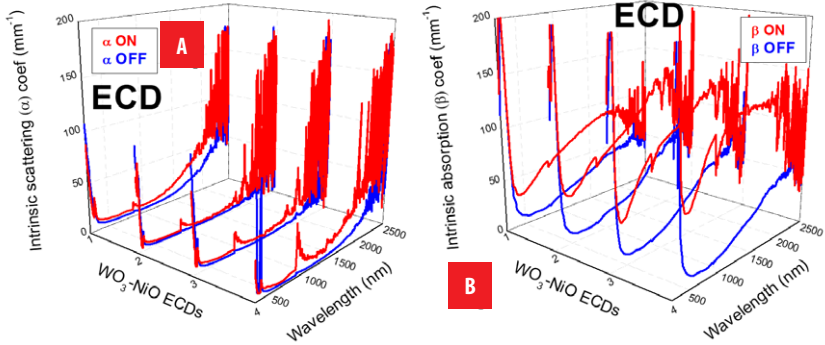


FIGURE 12: Intrinsic S&A-C: A α and B β (mm^{-1}).

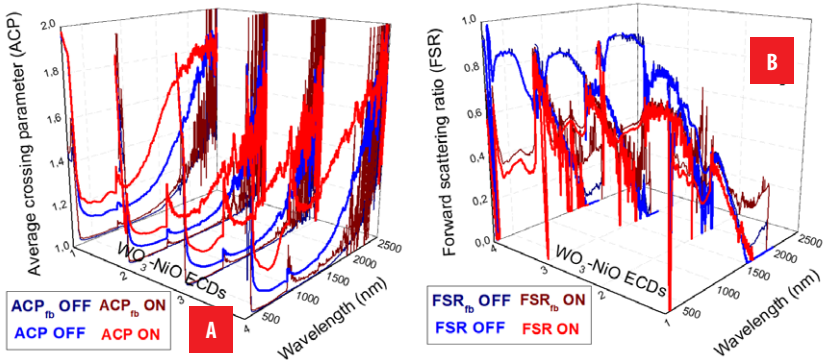


FIGURE 13: A ACP and ACP_{fb} B FSR and FSR_{fb}.

DISCUSSION

The onset of the discrepancies around 1500 nm precedes the spectral region where instrumental noise becomes significant. Therefore, the deviations observed between 1500 and 2000 nm are mainly attributed to the simplifying assumptions of the present single-layer implementation of the IJ-method, in which identical ACP and FSR values are assumed for both propagation directions and for both collimated and diffuse radiation. For wavelengths above approximately 2000 nm, the quality of the diffuse transmittance measurements is additionally affected by experimental noise. This originates from the absence of a standard light trap (black cone) in the integrating sphere, which was replaced by black sandpaper, leading to increased fluctuations in the diffuse signal. This effect does not influence the reflectance measurements.

Beyond the internal consistency of the 4FM and 2FM formulations, it is important to position the present approach within the broader framework of optical modeling of electrochromic devices (ECDs). Conventional methods such as the transfer-matrix method (TMM) and effective medium theory (EMT) are widely used to describe multilayer optical systems. While these approaches provide rigorous solutions when the complex refractive indices and precise thicknesses of each layer are



known, they typically focus on coherent propagation and specular components. In contrast, the present 4FM formalism operates directly with radiometric quantities and explicitly separates collimated and diffuse contributions, allowing experimental validation without requiring detailed microscopic optical constants. This makes the method particularly suitable for practical ECD characterization, where scattering and absorption coexist and may vary with the EC state.

Furthermore, the distinction between intrinsic (4FM) and extrinsic (2FM) coefficients provides additional diagnostic value. The intrinsic formulation captures the full internal radiative transport within the multilayer structure, whereas the extrinsic approximation neglects higher-order internal interactions. The discrepancy between both formulations therefore quantifies the impact of multiple scattering and nonlinear absorption effects, especially under strong coloration (COOS). This separation is not merely mathematical but offers a practical tool to identify performance limitations and to guide multilayer optimization strategies in ECD design. Overall, these results demonstrate that the IJ-based 4FM formulation not only reproduces the spectral response of electrochromic multilayer devices with high accuracy in the 250–1500 nm range, but also provides physically interpretable intrinsic parameters that enable separation of absorption and scattering mechanisms and quantitative assessment of multilayer coupling effects. This dual capability distinguishes the present approach from conventional purely coherent optical models and highlights its relevance for practical ECD analysis and optimization.

To predict the optical appearance of the four ECDs from the T data of the isolated WO_3 and NiO EC active layers shown in Fig. 4a [31, 33], the T of the four ECD was calculated in Fig. 16 over the visible wavelength range (VWR) using the approximation $T_{AB^i} = T_{A^i} \cdot T_{B^i}$, described at the last paragraph of the Introduction. The approximated T were then compared with the measured T_{reg} values of Fig. 5a (also plotted in Fig. 14a for BOOS and in Fig. 14b for COOS, together with the excellent agreement in fittings). Neglecting the glass, FTO, and electrolyte layers, as well as the R of the EC WO_3 and NiO active layers, the approximation assumed $T_{AB^i} = T_{A^i} \cdot T_{B^i}$, where T_{A^i} corresponds to WO_3 (single or double) and T_{B^i} to NiO (single or double). The T of double-thickness layers was obtained as the square of the single-thickness T, i.e., $T_{B^2} = T_{B^1} \cdot T_{B^1}$ for the BOOS and $T_{C^2} = T_{C^1} \cdot T_{C^1}$ for the COOS, as shown in Figs. 16a and 16b for WO_3 and NiO, respectively. In this way, T_{B^1} , T_{B^2} , T_{C^1} and T_{C^2} are the T of constructed single layer (T_{B^1} and T_{C^1}) and of simulated double layers (T_{B^2} and T_{C^2}) for separated EC layers, i.e., for WO_3 in Fig. 16a and for NiO in Fig. 16b. These T_{A^i} and T_{B^i} values were then used to approximate the calculated T shown in Fig. 16c ($T_X^{11} = T_X^1 \cdot T_X^1$, $T_X^{12} = T_X^1 \cdot T_X^2$, $T_X^{21} = T_X^2 \cdot T_X^1$ and $T_X^{22} = T_X^2 \cdot T_X^2$, with $x = b$ for BOOS and $x = c$ for COOS). To test the approximation $T_{AB^i} = T_{A^i} \cdot T_{B^i}$, the calculated T shown in Fig. 16c can be compared with the measured T spectra in Fig. 16d (in Fig. 5a and in Fig. 14a and 14b for the SWR), for ECD11, ECD12, ECD21, and ECD22).

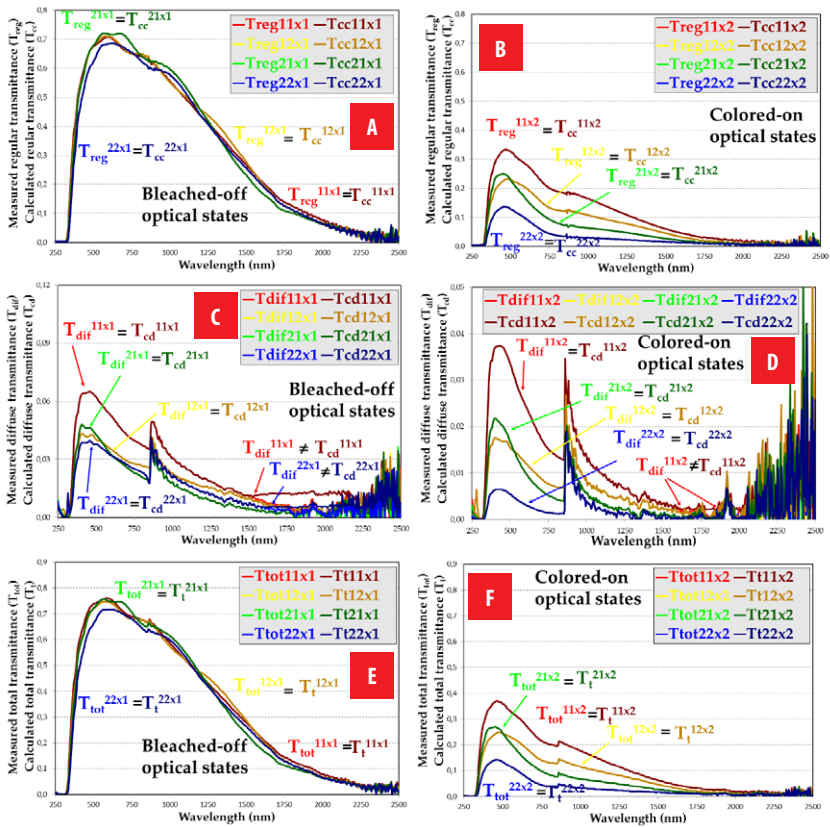


FIGURE 14: Measured and calculated T of the four WO_3 -NiO ECDs: BOOS **A** and COOS **B** regular T , BOOS **C** and COOS **D** diffuse T , and BOOS **E** and COOS **F** total T . Discrepancies only between T_{dif} and T_{cd} for ECD11 and ECD22 samples.

From the measured collimated T (T_{reg}) shown in Fig. 16 for the VWR, the CIE 1931 xy chromaticity coordinates of the four WO_3 -NiO ECDs for both BOOS and COOS were determined and presented in Fig. 17. For separated EC layers, T values of Fig. 16a and 16b are used to determine the CIE 1931 xy values for BOOS1, BOOS2, COOS1 and COOS2, of Fig. 17a and Fig. 17b, respectively. Concerning the ECDs, for the calculated cases, the BOOS11, BOOS12, BOOS21 and BOOS22 (of Fig. 17c) and the COOS11, COOS12, COOS21 and COOS22 (of Fig. 17d) were determined with the T_b^{11} , T_b^{12} , T_b^{21} and T_b^{22} and the T_c^{11} , T_c^{12} , T_c^{21} and T_c^{22} of Fig. 16c. In the same way, for the measured cases, the CIE 1931 xy values of Fig. 17e and Fig. 17f were determined with the data of Fig. 16d. Comparison of the calculated with the approximation and the measured ECDs can be carried out with Fig. 16c and Fig. 16d, for T data, and with Fig. 17c and Fig. 17e, for BOOS and with Fig. 17d and Fig. 17f, for COOS, for CIE 1931 chromaticity values.

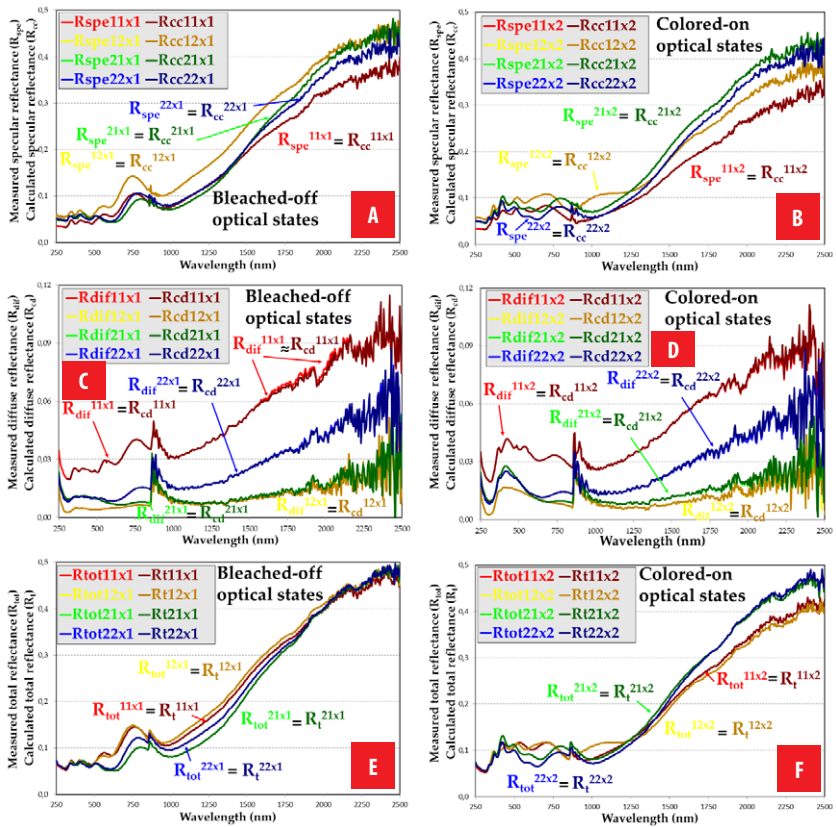


FIGURE 15: Measured and calculated R of the four WO₃-NiO ECDs: BOOS **A** and COOS **B** specular R, BOOS **C** and COOS **D** diffuse R, and BOOS **E** and COOS **F** total R. No discrepancies between measured and calculated R.

Given that the IJ method employed in this study for the 4FM provides reliable agreement within 250–1500 nm wavelength range, the determination of the intrinsic scattering and absorption coefficients (S&A-C) for the four ECDs, treated as a single layer in their sandwich configuration, must be considered approximate. The extrinsic S&A-C values should also be regarded as approximations, since the original 2FM was formulated for purely diffuse light propagation [16], owing to the two-flux structure of its governing differential equations. However, it was later suggested that the method can be reasonably extended to samples in which collimated T&R components coexist with diffuse T&R [20]. In any case, because the 4FM incorporates four fluxes instead of two, thereby accounting for additional radiative information, it can be considered, in principle, more accurate than the 2FM. Accordingly, Table 1 reports values averaged over the VWR, weighted by the human eye sensitivity curve, i.e., the CIE 1931 standard observer color matching function \bar{y} (2°). The numerical values in Table 1 indicate that, for the COOS, the increase in both the intrinsic and extrinsic absorption coefficients is greater for ECD21 than for ECD12; that is, doubling the thickness of WO₃ produces a larger effect than doubling the thickness of NiO.

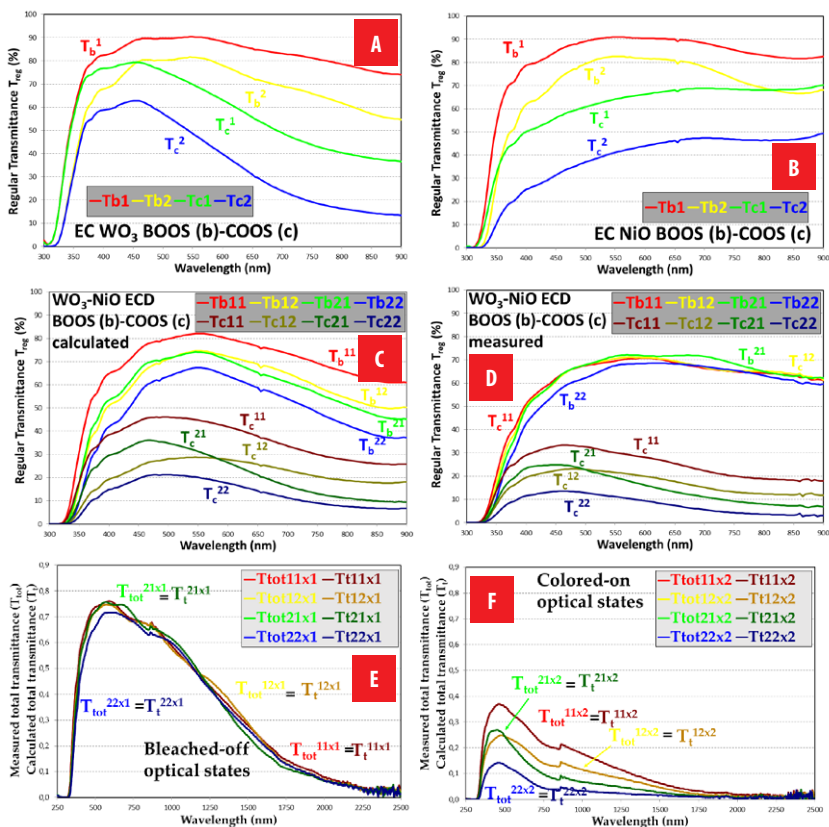


FIGURE 16: Regular T of the separated electrochromic layers and calculated and measured T for BOOS and COOS. Separated WO_3 **A** and NiO **B**. Calculated T, neglecting R of separated WO_3 and NiO layers, **C**, and measured T, of ECD11, ECD12, ECD21 and ECD22 **D**.

TABLE 1: Visible averaged values of intrinsic (α & β) and extrinsic (S & K) scattering and absorption coefficients and of imaginary part of refractive index (κ) obtained for ECD11, ECD12, ECD21 and ECD22, for BOOS and COOS.

Sample Parameter	BOOS ECDs				COOS ECDs			
	1	2	3	4	1	2	3	4
α (mm^{-1})	4.3839	2.1851	2.3764	2.4502	7.5006	4.4019	4.9746	4.8205
β (mm^{-1})	7.2558	8.1277	8.7753	10.8760	34.7830	49.2670	54.4340	77.2810
S (mm^{-1})	1.2236	0.0253	0.2614	0.3603	3.6464	1.7001	2.1008	3.0212
K (mm^{-1})	7.3049	8.1200	8.7977	77.7390	35.2960	49.5380	54.7960	77.7390
κ	0.0050	0.0045	0.0048	0.0058	0.0185	0.0235	0.0261	0.0360

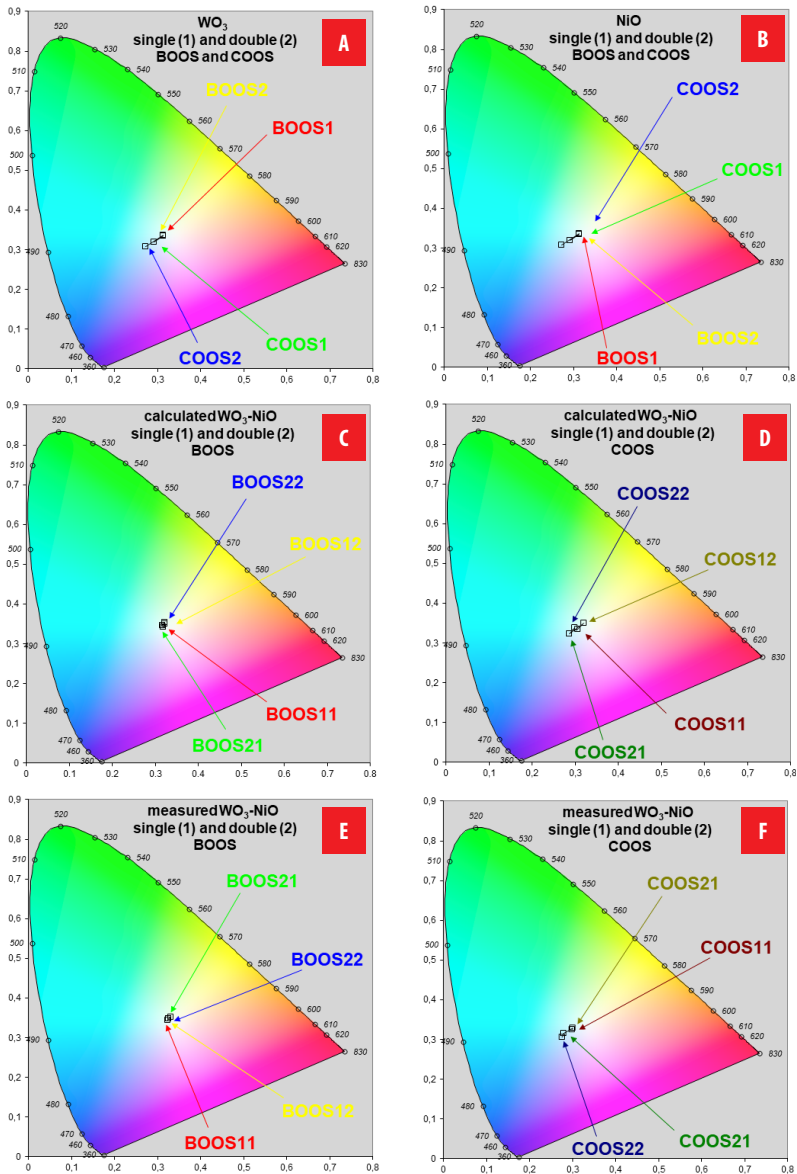


FIGURE 17: CIE 1931 xy chromaticity diagrams for single and double of separated EC layers at BOOS and COOS **A** WO_3 , **B** NiO, and of the complete ECDs **C** calculated BOOS, **D** calculated COOS, **E** measured BOOS and **F** measured COOS.

From the CIE XYZ tristimulus values [34, 35], the sRGB color representations of the four measured ECDs were computed and are displayed in Fig. 18. Accordingly, these results are compared with the calculated colors derived from the approximation, which neglects effects of the outer glass and FTO outer and the inner electrolyte layers, and the R

contributions of the individual WO_3 and NiO active layers. In this way, colors of inner squares of Fig. 18 were previously shown in the last two rows of Fig. 4d corresponding to WO_3 & NiO. The numerical data corresponding to Figs. 17 and 18 are summarized in Table 2.

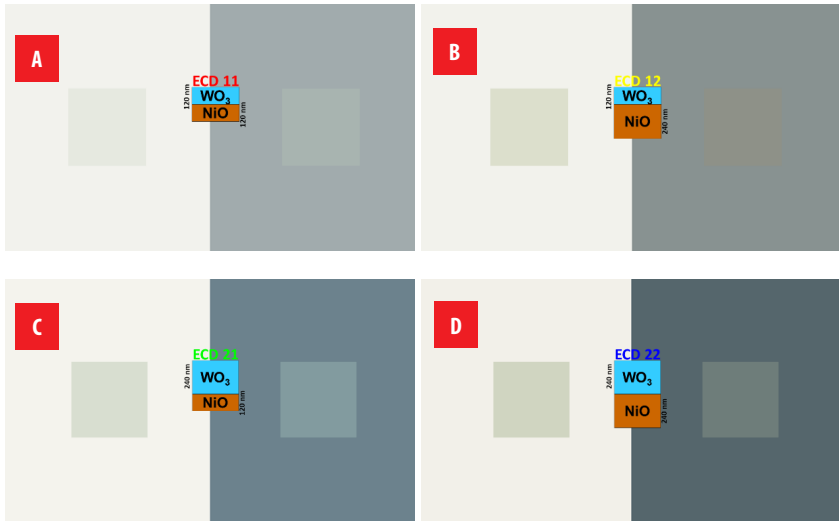


FIGURE 18: Comparison of the color perception from the determined sRGB values for the four WO_3 -NiO ECDs **A** ECD11, **B** ECD12, **C** ECD21 and **D** ECD22, for BOOS and COOS. The inner small square is related to the approximated values.

Note that the values listed in Table 2 correspond to the WO_3 and NiO samples with 120 nm thicknesses, whose T_{dir} spectra are shown in Fig. 4, and to the ECD11, ECD12, ECD21, and ECD22 devices, whose T_{reg} spectra are presented in Fig. 5a. The remaining samples are fictitious, obtained by assuming double thicknesses for WO_3 and NiO—denoted WO_3^2 and NiO^2 —and represented as squares following the approximation $T_{AB} = T_A \cdot T_B$. These fictitious configurations correspond to the ECD11 (WO_3 -NiO), ECD12 (WO_3 -NiO²), ECD21 (WO_3^2 -NiO), and ECD22 (WO_3^2 -NiO²). In these representations, the additional layers of the sandwich structure—namely, the outer glass substrates, the FTO TC coatings, and the internal electrolyte—were neglected. The R of the individual WO_3 and NiO layers was also disregarded, since only their T was considered. The differences in sRGB values between the measured and fictitious ECDs are smaller for the BOOS than for the COOS, as it can be deduced in Fig. 18. For the BOOS, the percentage deviations in R, G, and B coordinates were calculated as follows: 4.30%, 6.25%, and 7.03% for ECD11; 0.39%, 1.95%, and 1.17% for ECD12; -2.34%, 1.56%, and 2.34% for ECD21; and -4.30%, 0.00%, and -0.39% for ECD22. For the COOS, the corresponding values were 11.33%, 11.33%, and 8.59% for ECD11; 8.98%, 6.25%, and 1.95% for ECD12; 10.94%, 11.72%, and 8.20% for ECD21; and 12.11%, 11.33%, and 7.42% for ECD22. These differences were computed by subtracting the sRGB values of the fictitious samples from those of the measured ones and dividing by 256 (the number of discrete sRGB intensity levels).



TABLE 2. CIE 1931 xy and sRGB values of single and double samples WO_3 , NiO, WO_3 -NiO, WO_3 -NiO², WO_3^2 -NiO, WO_3^2 -NiO², ECD11, ECD12, ECD21 and ECD22, for BOOS and COOS.

Sample	CIE 1931 xy for BOOS		CIE 1931 xy for COOS		sRGB values for BOOS			sRGB values for COOS		
	x	y	x	y	R	G	B	R	G	B
WO_3	0.3133	0.3341	0.2928	0.3193	240	244	239	199	220	229
WO_3^2	0.3127	0.3372	0.2734	0.3070	226	233	225	154	190	207
NiO	0.3187	0.3392	0.3282	0.3455	244	244	234	215	208	194
NiO ²	0.3235	0.3472	0.3426	0.3589	233	234	216	181	170	148
WO_3 -NiO	0.3181	0.3423	0.3064	0.3347	230	233	221	168	180	176
WO_3 -NiO ²	0.3228	0.3502	0.3203	0.3491	220	223	204	142	146	134
WO_3^2 -NiO	0.3174	0.3453	0.2862	0.3230	216	223	208	130	155	158
WO_3^2 -NiO ²	0.3221	0.3532	0.2993	0.3383	207	213	192	110	125	121
ECD11	0.3238	0.3447	0.2985	0.3248	219	217	203	139	151	154
ECD12	0.3250	0.3475	0.3011	0.3298	219	218	201	119	130	129
ECD21	0.3307	0.3517	0.2803	0.3149	222	219	202	102	125	137
ECD22	0.3263	0.3481	0.2754	0.3067	218	213	193	79	96	102

The overall sRGB color distance, defined as the Euclidean distance between the R, G, and B components, yielded the following results: for BOOS, 10.34% (ECD11), 2.31% (ECD12), 3.66% (ECD21), and 4.31% (ECD22); and for COOS, 18.18% (ECD11), 11.12% (ECD12), 18.01% (ECD21), and 18.17% (ECD22). The relatively low color distances obtained for BOOS (< 10%) indicate that the approximation is reasonably accurate when predicting the optical appearance of the devices in their uncolored state (BOOS). The larger deviations observed for COOS suggest that the simplifications—namely, neglecting the optical effects of glass, FTO, electrolyte, and layer R—become less valid when the devices are colored. This occurs because, in COOS, the active layers develop stronger and narrower spectral absorption and scattering features. Small spectral shifts or shape variations thus lead to larger perceptual color differences. Furthermore, nonlinear interactions between layers (e.g., multiple reflections, interference, and interfacial coupling) become more significant when absorption increases, amplifying the discrepancies between the measured and approximated results.

CONCLUSIONS

In this work, the optical constants (OC) and the intrinsic and extrinsic scattering and absorption coefficients (S&A-C) of four WO_3 -NiO electrochromic devices (ECD) were determined for all combinations of single and double active-layer thicknesses, at both bleached-off (BOOS) and colored-on (COOS) optical states. The study followed a single-layer procedure previously validated for suspended particle devices (SPD) [13] and polymer-dispersed liquid crystals (PDLC) [14, 15]. The OC (n and k), derived from the



collimated–collimated (T_{cc} and R_{cc}) equations of the four-flux model (4FM), were used to compute the collimated intermediate parameters (r_c and ϵ), from which the extrinsic and intrinsic S&A-C were subsequently obtained. Extrinsic S&A-C were calculated using the Kubelka–Munk two-flux model (KM-2FM) and the Saunderson correction for interfaces. However, when total transmittance and reflectance measurements (T&R-M) are used instead of diffuse ones, the approximation may become inaccurate for low-haze samples such as ECDs, where total and diffuse T&R-M components differ significantly. Moreover, the diffuse transmittance at longer wavelengths was measured with significant noise due to the absence of a proper light trap (black cone) in the integrating-sphere-based spectrometer, which is typically used to absorb diffuse radiation (i.e., acting as a light sink). In our setup, this component had to be improvised using black sandpaper. Consequently, the noisy diffuse T measurements led to increased uncertainty in the retrieved S and K values at longer wavelengths (>2000 nm). Similarly, intrinsic S&A-C determined from the collimated–diffuse 4FM equations (T_{cd} and R_{cd}) are less reliable above 1500 nm, since the same average crossing parameter (ACP) and forward scattering ratio (FSR) are assumed for both forward and backward propagation, and for both collimated and diffuse radiation.

The inverse scattering and absorption problem aims to determine the intrinsic (4FM) and extrinsic (2FM) S&A-C from T&R-M, thereby inferring the size, shape, and composition of the particles responsible for light scattering and absorption [36]. The original differential equations of the 4FM were formulated in [37]. The first analytical 4FM solutions proposed in [19] were complemented by the RT-method (see Introduction), which introduced a fifth equation for the ACP parameter. Later, this RT-method [31, 32] was replaced by the IJ-method [13, 14, 15], which uses forward (i) and backward (j) light intensities instead of T and R. In this study, the IJ-method was applied as the fifth equation required to solve the system of four equations (T_{cc} , R_{cc} , T_{cd} , R_{cd}) and five unknowns (n , κ , α , ACP, FSR), since $\beta = \epsilon - \alpha$. The IJ-method was later extended into the directed-IJ-method [38, 39], introducing two ACP parameters (for forward and backward propagation) and four FSR parameters (for forward/backward and collimated/diffuse radiation). In this case, $\text{ACP} = 1 + q$, i.e., $\text{ACP}^i = 1 + q^i = 1 + i\alpha^0 / \rho$ and $\text{ACP}^j = 1 + q^j = 1 + j\alpha^0 / \rho$.

The present results can be improved in future work by applying the newly developed equations for intrinsic S&A-C from the diffuse differential equations of the 4FM [38] and extrinsic S&A-C from the total differential equations of the 2FM [38, 39]. The new 2FM equations are valid for any haze level, since they are derived by expressing the total differential equations of the 2FM as the sum of the collimated and diffuse differential equations of the 4FM [39] for each propagation direction. These new formulations have already been applied to single-layer studies of SPD and PDLC samples [40, 41], within a three-substrate-layer sandwich structure (TSLSS), and to black coating paints used in solar thermal collectors [42]. That approach enforced a three-extinction matching requirement ($3\epsilon\text{MR}$) [38, 39], enabling thickness-gradient plots (TGP) even in samples approximated with fewer layers.

For the present WO_3/NiO ECDs, the seven-layer sandwich structure was simplified into a single substrate layer sandwich structure including the front and rear glass substrates, and an internal composite layer that includes the transparent conductor, electrolyte, and WO_3/NiO active films. Future work will aim to increase the number of modeled layers to



refine these approximations and to implement the directed IJ-method instead of the non-directed version used in the current analysis. A recent study applied the TSLSS configuration and a novel procedure—previously used to enforce the $3\epsilon\text{MR}$ in SPD and PDLC samples [43]—to the four inorganic ECDs analyzed in this work [44]. However, it would be more informative to extend this analysis from three to seven layers, allowing separate evaluation of the WO_3 and NiO active films while explicitly considering the FTO [8] and electrolyte [38, 39] contributions. For this purpose, the spectral limit of the optical behavior between film and substrate (SLOBFS) is currently under investigation in WO_3 -FTO-glass and NiO-FTO-glass three-layer samples with three different WO_3 thicknesses—single, double, and quadruple. These samples are analyzed only in the BOOS, since for the COOS they must be assembled as complete ECDs. Nevertheless, some insights for the COOS of these WO_3 -FTO-glass and NiO-FTO-glass configurations may be inferred from Fig. 4 of the present work. The SLOBFS are hypothesized to occur at shorter wavelengths for the interfaces between WO_3 and FTO (for both single and double WO_3 layers) and between NiO and FTO, corresponding to a transition from substrate-substrate-substrate (SSS) to film-substrate-substrate (FSS) configurations. Subsequently, the SLOBFS between FTO and glass—previously observed at around 1200 nm, approximately three times the FTO layer thickness— would correspond to a transition from FSS to film-film-substrate (FFS) configurations. Finally, for the quadruple WO_3 layer, two further transitions, first from SSS to substrate-film-substrate (SFS) configuration (at 1200 nm, corresponding to the SLOBFS of FTO of 400 nm), and then from SFS to FFS configuration (at 1440 nm, corresponding to the SLOBFS of FTO of 400 nm), was preliminarily observed [45].

For future work, the determination of the optical constants and the intrinsic and extrinsic S&A-C of the individual WO_3 and NiO electrochromic layers in their bleached and colored optical states (BOOS and COOS) would require new measurements on additional ECD samples. This is necessary because, due to the non-symmetrical sandwich structure (G-FTO- WO_3 -E-NiO-FTO-G), the optical characterization must be performed in both orientations, i.e., also in the reversed configuration (G-FTO-NiO-E- WO_3 -FTO-G). As the primary electrochromic material, WO_3 can be combined not only with NiO but also with other complementary electrochromic materials [46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58]. Consequently, the parameters obtained from the three pairs of governing differential equations—namely, the four-flux formulation in the 4FM, which provides the OCs and the intrinsic S&A-C, and the two-flux formulation in the 2FM, which yields the extrinsic S&A-C—can be analyzed not only for the WO_3 /NiO system, but also for WO_3 coupled with other counter-electrode electrochromic materials employed in the fabrication of ECDs. In addition, the 400 nm thick FTO transparent conductive layer used in the present samples could be replaced by layers with different thicknesses or prepared using alternative deposition techniques, or even substituted by ITO or other transparent conductive materials [59, 60, 61, 62, 63, 64, 65, 66]. In addition to the procedure based on the new equations for the intrinsic 4FM and extrinsic 2FM S&A-C described in previous works [38, 39, 40, 41, 42, 43, 44], alternative methodologies could also be implemented in order to compare and validate the results [66 - 108].

APPENDIX: NOMENCLATURE

Greek symbols

α	intrinsic scattering coefficients
β	intrinsic absorption coefficients
δ	z coordinate at front interface
ε	extinction coefficient
κ	imaginary part of refractive index
λ	wavelength
θ_c	critical angle for total internal reflection
ω	interface reflectance

English symbols

0	z coordinate at back interface
2FM	two-flux model
3 ε MR	three extinction matching requirement
4FM	four-flux model
ACP	average crossing parameter
BOOS	bleached-off optical state
COOS	colored-on optical state
cc	collimated-collimated
cd	collimated-diffuse
ECD	electrochromic device
FSR	forward scattering ratio
fb	feedback
FSS	film-substrate-substrate
FFS	film-film-substrate
FTO	fluorine-doped tin oxide
i	forward light flux
i^0	forward light flux at the back interface
i^δ	forward light flux at the front interface
i_c	collimated forward light flux
i_c^0	collimated forward light flux at the back interface
i_c^δ	collimated forward light flux at the front interface
i_d^0	diffuse forward light flux at the back interface
i_d^δ	diffuse forward light flux at the front interface
ITO	tin-doped indium oxide
IJ	forward light flux-backward light flux
j	backward light flux
j^0	backward light flux at the back interface
j^δ	backward light flux at the front interface
j_c	collimated backward light flux at the front interface



j_c^0	collimated backward light flux at the back interface
j_c^δ	collimated backward light flux
j_d^0	diffuse backward light flux at the back interface
j_d^δ	diffuse backward light flux at the front interface
K	extrinsic absorption coefficient
KM	Kubelka-Munk
MLG	Maheu-Letoulozan-Gouesbet
n	real part of refractive index
\tilde{n}	complex refractive index
NiO	nickel oxide
OC	optical constants
PDLC	polymer dispersed liquid crystal
q	diffuse fraction of light
q_0^i	diffuse fraction of the forward light at the back interface
q_0^j	diffuse fraction of backward light at the front interface
R	reflectance
R_b	reflectance at the bleached-off optical state
R_c	reflectance at the colored-on optical state
r_c	collimated interface reflectance
r_d	diffuse interface reflectance
r_d^e	external diffuse interface reflectance
r_d^i	internal diffuse interface reflectance
R_{spe}	measured specular reflectance
R_{cc}	calculated specular reflectance
R_{dif}	measured diffuse reflectance
R_{cd}	calculated diffuse reflectance
R_t	calculated total reflectance
R_{tot}	measured total reflectance
RT	reflectance-transmittance
S	extrinsic scattering coefficient
SFS	substrate-film-substrate
SSS	substrate-substrate-substrate
SWR	solar wavelength range
SLOBFS	spectral limit of the optical behavior between film and substrate
S&A-C	scattering and absorption coefficients
SPD	suspended particle device
T	transmittance
T_b	transmittance at the bleached-off optical state
T_c	transmittance at the colored-on optical state
T_{cc}	calculated specular transmittance
T_{reg}	measured regular transmittance



T_{cd}	calculated diffuse transmittance
T_{dif}	measured diffuse transmittance
T_t	calculated total transmittance
T_{tot}	measured total transmittance
TGP	thickness gradient plots
TSLSS	three-substrate layer sandwich structure
VWR	visible wavelength range
WO ₃	tungsten oxide

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AUTHORS' CONTRIBUTIONS

David Barrios carried out the measurements and wrote the manuscript; David Barrios and Carlos Alvarez performed 3D figures; David Barrios and Jose Miguitama found the key reference for computing properly the diffuse interface reflectance; David Barrios and Fabrizio Armando Lopez-Vargas determined the colorimetric results.

AI STATEMENT

No AI tools were used for scientific content generation, data analysis, or interpretation. All scientific results, analysis, and conclusions are the sole responsibility of the authors.

DATA AVAILABILITY STATEMENT

Data are available upon reasonable request to the corresponding author (in exceptional cases).

CONFLICT OF INTEREST

Authors declare that they have no conflicts of interest in this research.

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